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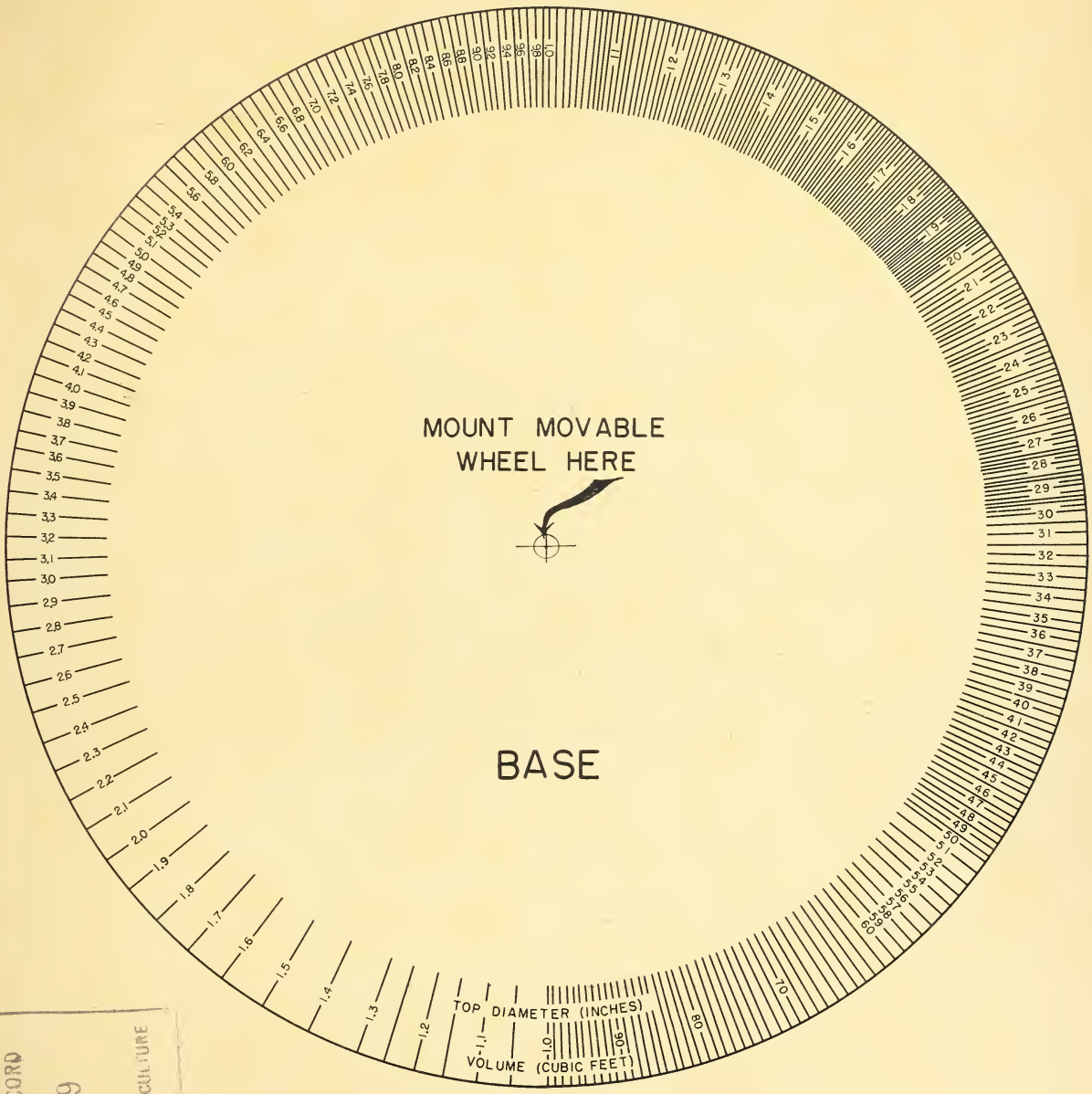
³
X A Method of
Estimating
Cubic Volume
in Felled Trees, X

2
by Frederick E. Hampf, & C. Allen Bickford

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7/26/55
STATION PAPER NO. 1171 • ^{7a} NORTHEASTERN FOREST EXPERIMENT STATION, 1959
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CIRCULAR SLIDE RULE A FOR CUBIC VOLUME IN 8-FOOT BUTT SECTION



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For use with "A method of estimating cubic volume in felled trees", by Frederick E. Hampf and C. Allen Bickford. (U.S. Forest Service Northeast. Forest Expt. Sta., Sta. Paper 117, 1959.)

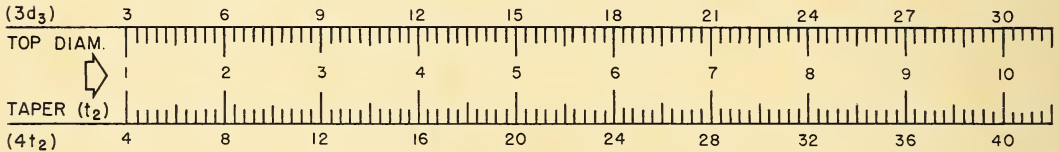
HOW TO OBTAIN THE TAPER FACTOR ($3d_3 + t_1 + 4t_2$)
FOR BUTT SECTION OF BUTT LOG

1. Measurements needed are inside-bark diameters at: (1) butt end, (2) 4.075-feet, (3) 8.15 feet.
2. Triple-top-diameter ($3d_3$) is obtained by reading up from the appropriate top diameter (at 8.15 feet) on the diagram.
3. Four times upper taper ($4t_2$) is obtained by reading down from the appropriate taper for the upper 4-foot section.
4. Taper factor is obtained by adding the values of ($3d_3$), ($4t_2$), and the taper of the 8-foot butt section (t_1).

EXAMPLE: ($3d_3$) for 21.2 inch top diam. is 63.6 inches.
($4t_2$) for upper taper of 2.2 inches is 8.8 inches.

Taper for entire butt section (t_1) is 8.4 inches.
Therefore, taper factor = $63.6 + 8.8 + 8.4 = 80.8$ inches.

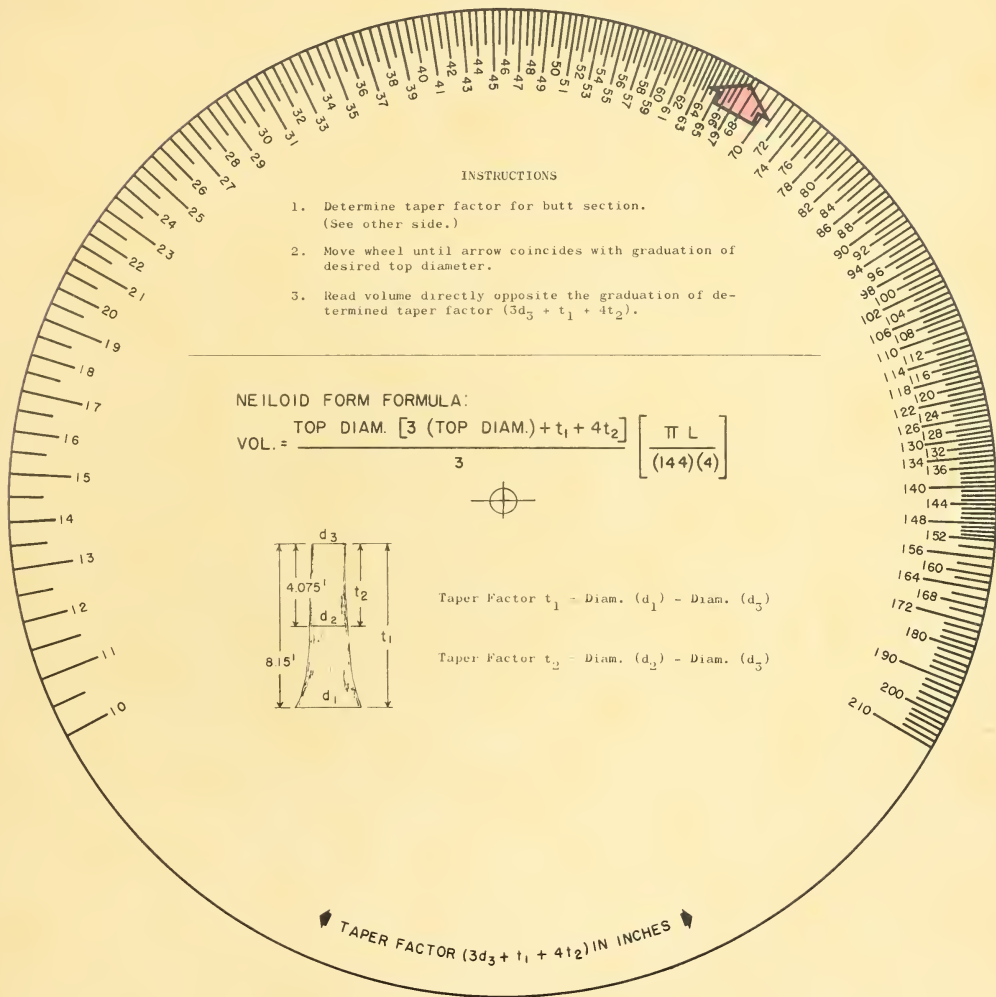
Volume for 8-foot length = 25.4 cubic feet.



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Movable wheel for Circular Slide Rule A.

Cut this out and mount on Base with metal grommet, binder post, or pin.



For use with "A method of estimating cubic volume in felled trees", by Frederick E. Hampf and C. Allen Bickford. (U.S. Forest Service Northeast. Forest Expt. Sta., Sta. Paper 117, 1959.)

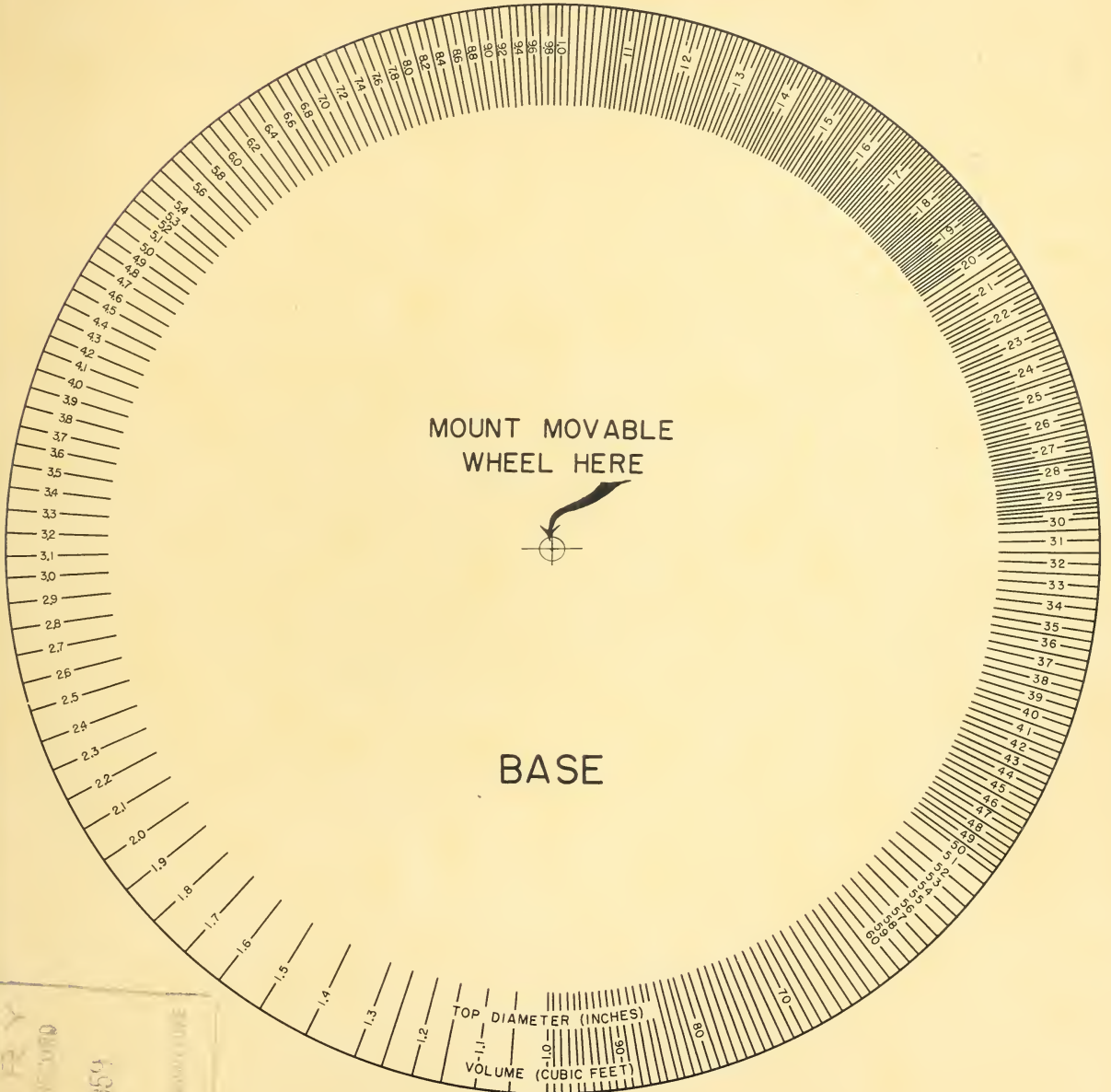
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CIRCULAR SLIDE RULE B FOR CUBIC VOLUME IN UPPER LOGS: 16-FOOT LENGTH



For use with "A method of estimating cubic volume in felled trees", by Frederick E. Hampf and C. Allen Bickford. (U.S. Forest Service Northeast. Forest Expt. Sta., Sta. Paper 117, 1959.)

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REDUCTION FACTORS, AT 0.1 - FOOT INTERVALS:

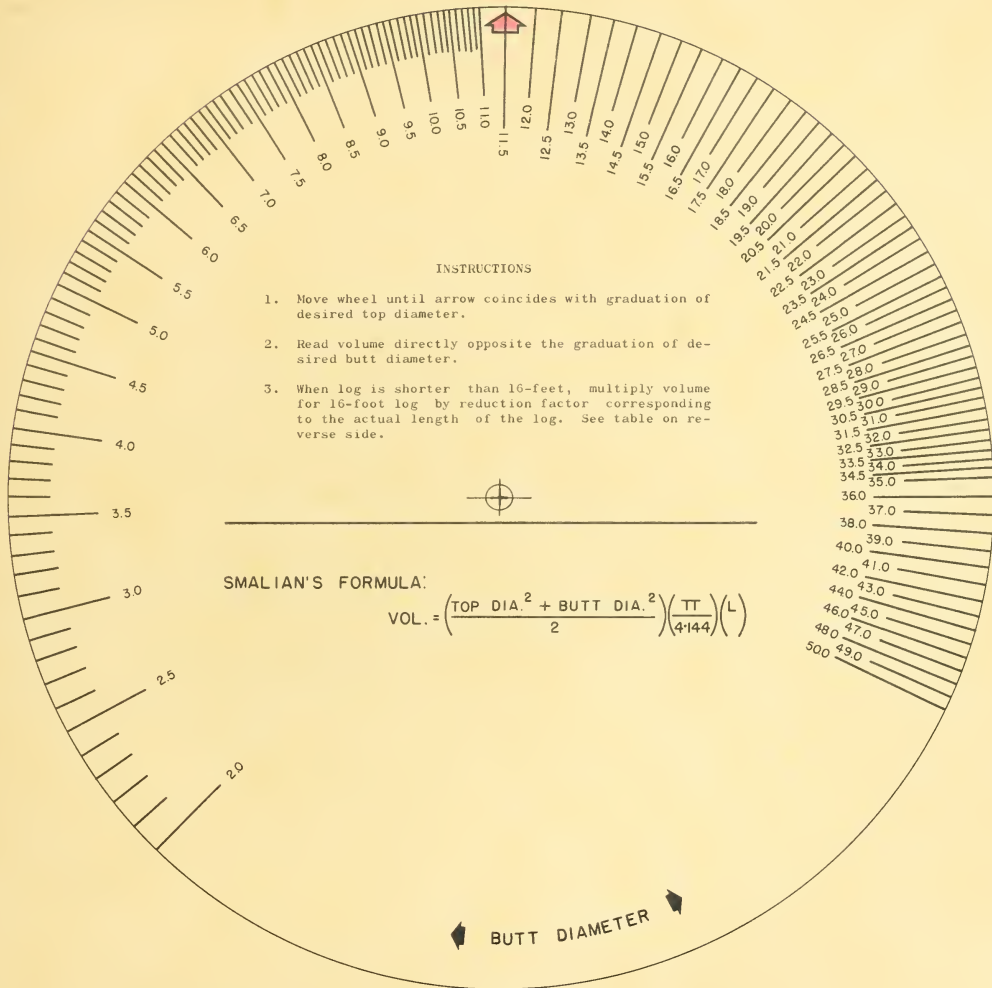
| Log length (feet) | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
|----------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0 | -- | 0.0062 | 0.0125 | 0.0188 | 0.0250 | 0.0312 | 0.0375 | 0.0438 | 0.0500 | 0.0562 |
| 1 | 0.0625 | .0688 | .0750 | .0812 | .0875 | .0938 | .1000 | .1062 | .1125 | .1188 |
| 2 | .1250 | .1312 | .1375 | .1438 | .1500 | .1562 | .1625 | .1688 | .1750 | .1812 |
| 3 | .1875 | .1938 | .2000 | .2062 | .2125 | .2188 | .2250 | .2312 | .2375 | .2438 |
| 4 | .2500 | .2562 | .2625 | .2688 | .2750 | .2812 | .2875 | .2938 | .3000 | .3062 |
| 5 | .3125 | .3188 | .3250 | .3312 | .3375 | .3438 | .3500 | .3562 | .3625 | .3688 |
| 6 | .3750 | .3812 | .3875 | .3938 | .4000 | .4062 | .4125 | .4188 | .4250 | .4312 |
| 7 | .4375 | .4438 | .4500 | .4562 | .4625 | .4688 | .4750 | .4812 | .4875 | .4938 |
| 8 | .5000 | .5062 | .5125 | .5188 | .5250 | .5312 | .5375 | .5438 | .5500 | .5562 |
| 9 | .5625 | .5688 | .5750 | .5812 | .5875 | .5938 | .6000 | .6062 | .6125 | .6188 |
| 10 | .6250 | .6312 | .6375 | .6438 | .6500 | .6562 | .6625 | .6688 | .6750 | .6812 |
| 11 | .6875 | .6938 | .7000 | .7062 | .7125 | .7188 | .7250 | .7312 | .7375 | .7438 |
| 12 | .7500 | .7562 | .7625 | .7688 | .7750 | .7812 | .7875 | .7938 | .8000 | .8062 |
| 13 | .8125 | .8188 | .8250 | .8312 | .8375 | .8438 | .8500 | .8562 | .8625 | .8688 |
| 14 | .8750 | .8812 | .8875 | .8938 | .9000 | .9062 | .9125 | .9188 | .9250 | .9312 |
| 15 | .9375 | .9438 | .9500 | .9562 | .9625 | .9688 | .9750 | .9812 | .9875 | .9938 |

Example: 10.7-foot log, 13.1-inch top diameter, 14.8 inch butt diameter.
 Volume for 16-foot length = 17.0 cubic feet. Volume for 10.7-foot log = 17.0 x 0.6688 = 11.37 cubic

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Movable wheel for Circular Slide Rule B.

Cut this out and mount on Base with metal grommet, binder post, or pin.



For use with "A method of estimating cubic volume in felled trees", by Frederick E. Hampf and C. Allen Bickford. (U.S. Forest Service Northeast. Forest Expt. Sta., Sta. Paper 117, 1959.)

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X *A Method of*
Estimating
Cubic Volume
in Felled Trees X

2/
by Frederick E. Hampf & C. Allen Bickford

About the Authors...

FREDERIC E. HAMPF joined the U.S. Forest Service in 1937 following his graduation from the University of Idaho. He came to the Northeastern Forest Experiment Station in 1946. A specialist in mensuration, he has conducted a number of surveys on timber production and has made wood-utilization studies of stump diameter-d.b.h. relationships for a score of timber tree species. He is currently in charge of the timber-cut aspects of the Forest Survey in the Northeast.

C. ALLEN BICKFORD, forester and mathematical statistician at the Northeastern Forest Experiment Station since 1947, began his career in forest research with the Southern Forest Experiment Station in 1931. He took his B.S. degree at Dartmouth in 1925 and his Master's in forestry at the University of Idaho in 1931.

THIS paper describes a new method of computing the gross volume of felled trees or sections of trees. The method has many applications, but most are limited to forest research and management, especially in making surveys.

In a sense, this method is a compromise between the tedious but fairly accurate planimeter method and the faster but less accurate method of estimating by diameter (d.b.h.) volume tables. We feel that the method detailed here is twice as fast as measuring by planimeter and far more accurate than estimating by whole-tree volume tables.

It offers less chance of errors in human judgment and can mean fewer office computations. It has the easy practicality that foresters require, while approximating the accurate results--butt logs notwithstanding--of the xylometer, use of which is highly restricted.

This method is being used in wood-utilization studies for the Forest Survey in the Northeast. The Forest Survey reports the volume of timber cut from forests within a given state. This volume, expressed in cubic feet, includes timber cut and removed and also logging residues left in the woods, including trees destroyed by logging. These differences--between timber actually harvested and Forest Survey utilization standards--must also be determined to estimate the volume of timber cut.

Assumptions of Tree Form

To compute the total wood content of a tree one must assume that a tree is made up of certain geometric forms. For simplicity, we assume that the stump is a cylinder (fig. 1) with a diameter equal to its top diameter, inside bark, (average level or horizontal plane), and with a height of 1 foot from ground level (uphill side of tree).

We assume that the tree bole from 1 foot to 9.15 feet forms a frustum of a neiloid. Above this point the taper rate increases with height. Therefore, the upper bole, from 9.15 feet to the base of the crown, usually takes the general geometric form of the frustum of a paraboloid. We further assume that the top of fast-tapering single-stem trees forms the frustum of a cone.

Trees of unusual shape require special consideration. Each portion of such a tree should be fitted as circumstances require to the frustum of either a neiloid, paraboloid, cone, or cylinder.

Based on these assumptions, the measurements needed to compute total wood volume in a tree are diameter measurements at 1.00, 5.075, and 9.15 feet above ground level, at the upper end of each bucked section, and at the flexible 4-inch top.¹ Length measurements are needed for each section, including the stump and the portion of the top used above (or left below) the 4-inch top. Diameter measurements are taken to 0.1 inch, length to the nearest 0.1 foot.

Computations Required

Volumes of each of the log sections can be computed as follows:

Stump.--For Forest Survey purposes, only the volume of the stump between the assumed 1-foot height and actual stump height is necessary. Wood is "over-utilized" when a stump is cut below the 1-foot height, "under-utilized" when cut above it. Stump volume is obtained by multiplying the area (Appendix I, table 1) of the stump's top by the difference in height.

Butt log.--The lower 8-foot section of the 16-foot butt log is in the form of a neiloid frustum, and the upper portion of the butt log is in the form of a paraboloid frustum. Thus two steps are required to compute butt-log volume. Diameter measurements are needed at 1.00, 5.075, and 9.15 feet above ground level and at the top of the log. Volume of the butt 8-foot section is obtained from Circular Slide Rule A (Appendix II). Volume for the upper portion is obtained from Circular Slide Rule B (Appendix III), using diameters at 9.15 feet and log top.

Upper logs.--The cubic volume of 16-foot upper logs is obtained directly from Circular Slide Rule B. The volume of upper logs shorter than 16 feet is obtained as if they were 16-foot logs--then an appropriate reduction factor is applied. Reduction factors are given on the reverse side of Circular Slide Rule B.

¹To an obvious 4-inch top (d.i.b.) or to the point at which the main stem disappears because of branching.

Upper Stem.--The volume of over- or under-utilization (Forest Survey standards) of the upper stem is also required. This is the departure in cubic volume from the "flexible 4-inch top".

The upper stem in single-stem trees, which taper rapidly (no large and excessive branching) to an obvious 4-inch top d.i.b., generally approximates the form of a frustum of a cone.

The cubic volume for this portion of the tree is obtained from table 2 (Appendix IV). Greater accuracy may be got by subdividing any length in excess of 16 feet. The volume of this "butt" section is obtained from Circular Slide Rule B; the volume for the upper section is obtained from table 2.

Whenever abrupt taper occurs at localized points along the upper stem because of large or excessive branching, each section between these points should be considered as a frustum of a paraboloid, and its volume may be obtained from Circular Slide Rule B.

Limbs.--The cubic volume of all limbs utilized is also determined. Limb form is not parabolic but is assumed to be so for convenience; and limb volume, like that of upper logs, is obtained from Circular Slide Rule B. The limb's "butt" diameter should be measured away from and just below the point of noticeable knot swell. Once computed, this volume is over-utilization.

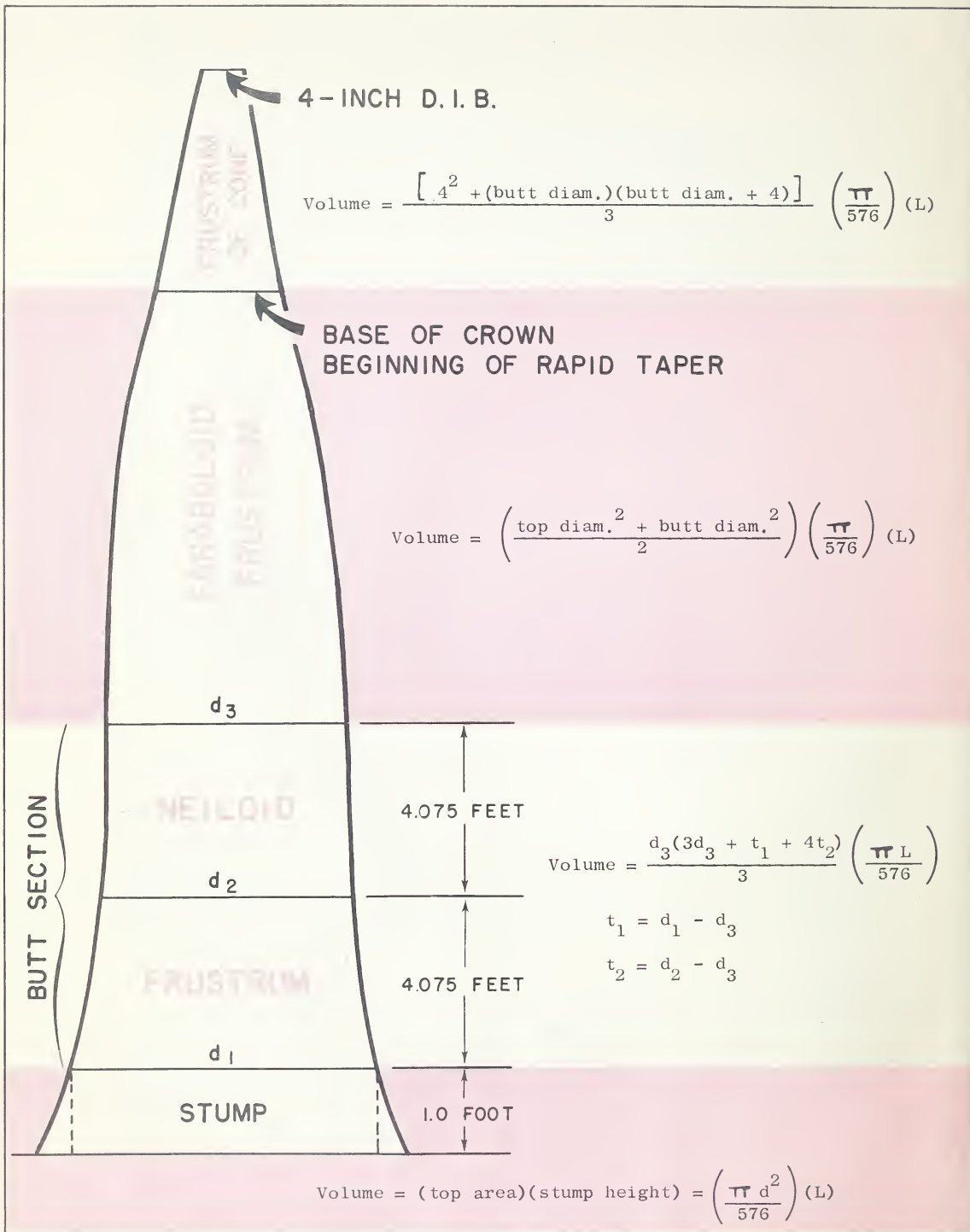
Example of Procedure

The following example shows how to compute the cubic volume for (1) the entire portion of a tree cut and removed and (2) the unutilized portion left in the woods. This computation is based on Forest Survey standards.

Measurements Of The Felled Tree

The tree was felled, leaving a stump 1.3 feet high and 25.4 inches in diameter. The tree's diameter measurements (inside bark) were:

| | <u>Inches</u> |
|------------------|---------------|
| at 1.00 foot -- | 26.0 |
| at 5.075 feet -- | 20.6 |
| at 9.15 feet -- | 19.9 |



The formula for determining the volume of a neiloid frustrum was derived from Newton's formula:

$$\text{Volume} = (B_1 + 4B_2 + B_3) \frac{L}{6}$$

$$= \left(\frac{d_1^2 + 4d_2^2 + d_3^2}{6} \right) \left(\frac{\pi L}{576} \right)$$

From the sketch:

$$t_1 = d_1 - d_3 \quad \text{or} \quad d_1 = d_3 + t_1 \quad \frac{\pi}{576} = \frac{3.1416}{576} = 0.005454\dots$$

$$t_2 = d_2 - d_3 \quad \text{or} \quad d_2 = d_3 + t_2 \quad L = 8.15 \text{ feet}$$

$$\text{Thus } d_1^2 + 4d_2^2 + d_3^2 = (d_3 + t_1)^2 + 4(d_3 + t_2)^2 + d_3^2$$

$$= 6d_3^2 + 2d_3(t_1 + 4t_2) + t_1^2 + 4t_2^2$$

And, as $t_1^2 + 4t_2^2$ is negligible in comparison with $6d_3^2 + 2d_3(t_1 + 4t_2)$

$$\text{Volume is approximately } \left(d_3^2 + \frac{d_3(t_1 + 4t_2)}{3} \right) \left(\frac{\pi L}{576} \right)$$

$$\text{Approximate volume of frustrum of neiloid} = \frac{d_3(3d_3 + t_1 + 4t_2)}{3} \left(\frac{\pi L}{576} \right)$$

Figure 1.--Tree forms and the formulas used to compute their cubic volume.

II. Determine volume of butt 8-foot section:

$$\begin{aligned} & 20.2 \text{ (from Circular Slide Rule A)} \\ & - \underline{1.06} \text{ (stump volume not harvested)} \\ & = 19.14 \text{ cubic feet} \end{aligned}$$

III. Determine volume of upper portion of butt log:

$$\begin{aligned} \text{Length of upper portion} &= 16.5 \text{ feet} - 8.2 \text{ feet (butt section)} \\ &= 8.3 \text{ feet} \end{aligned}$$

$$\begin{aligned} \text{Diameters of upper portion} &= 18.2 \text{ inches at top} \\ & 19.9 \text{ inches at 9.15 feet} \end{aligned}$$

$$\begin{aligned} \text{Volume as 16-foot log} \\ \text{(from Circular Slide Rule B)} &= 31.6 \text{ cubic feet} \end{aligned}$$

$$\begin{aligned} \text{Volume for 8.3-foot log} &= 31.6 \times 0.5188 \text{ (reduction factor} \\ \text{from Circular Slide Rule B)} &= 16.39 \text{ cubic feet} \end{aligned}$$

$$\text{IV. Volume of butt log} = 19.14 + 16.39 = \underline{35.53} \text{ cubic feet.}$$

3

Determine volume of 2nd log.

$$\begin{aligned} \text{Volume as a 16-foot log} \\ \text{(from Circular Slide Rule B)} &= 24.1 \text{ cubic feet} \end{aligned}$$

$$\text{Volume for 11.4-foot log} = 24.1 \times 0.7125 = \underline{17.17} \text{ cubic feet.}$$

4

Determine volume of 3rd log.

$$\begin{aligned} \text{Volume as a 16-foot log} \\ \text{(from Circular Slide Rule B)} &= 17.0 \text{ cubic feet.} \end{aligned}$$

$$\text{Volume for 10.7-foot log} = 17.0 \times 0.6688 = \underline{11.37} \text{ cubic feet.}$$

5

Determine volume of 4th log.

Volume as a 16 foot log
(from Circular Slide Rule B) = 12.1 cubic feet.

Volume for 8.4-foot log = $12.1 \times 0.5250 = \underline{6.35}$ cubic feet.

6

Determine total volume cut and removed from tree.

$35.53 + 17.17 + 11.37 + 6.35 = \underline{70.42}$ cubic feet.

Volume Of Upper Stem Left In The Woods

1

Volume of the upper stem "butt" section is obtained from Circular Slide Rule B, using diameters 10.2 and 7.4 inches and length 10.0 feet as follows:

Volume as 16-foot log = 6.6 cubic feet.

Volume for 10.0-foot log = $6.6 \times 0.6250 = 4.12$ cubic feet.

2

Determine volume of top's upper section (from table 2).

Interpolating:

volume for 7.4 inches x 10 feet long = 1.83 cubic feet.

Adjusting for length of 9.8 feet:

$(1.83) (0.98) = 1.79$ cubic feet.

3

Determine volume of top not utilized = $4.12 + 1.79$
= 5.91 cubic feet.

APPENDIX

I

Table 1.--Areas of circles, in square feet, for diameters in tenths of inches

| Diameter Inches | Tenths of inches | | | | | | | | | |
|--------------------|------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | 0.0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| 5 | 0.136 | 0.142 | 0.147 | 0.153 | 0.159 | 0.165 | 0.171 | 0.177 | 0.183 | 0.190 |
| 6 | .196 | .203 | .210 | .216 | .233 | .230 | .238 | .245 | .252 | .260 |
| 7 | .267 | .275 | .283 | .291 | .299 | .307 | .315 | .323 | .332 | .340 |
| 8 | .349 | .358 | .367 | .376 | .385 | .394 | .403 | .413 | .422 | .432 |
| 9 | .442 | .452 | .462 | .472 | .482 | .492 | .503 | .513 | .524 | .535 |
| 10 | .545 | .556 | .567 | .579 | .590 | .601 | .613 | .624 | .636 | .648 |
| 11 | .660 | .672 | .684 | .696 | .709 | .721 | .734 | .747 | .759 | .772 |
| 12 | .785 | .799 | .812 | .825 | .839 | .852 | .866 | .880 | .894 | .908 |
| 13 | .922 | .936 | .950 | .965 | .979 | .994 | 1.009 | 1.024 | 1.039 | 1.054 |
| 14 | 1.069 | 1.084 | 1.100 | 1.115 | 1.131 | 1.147 | 1.163 | 1.179 | 1.195 | 1.211 |
| 15 | 1.227 | 1.244 | 1.260 | 1.277 | 1.294 | 1.310 | 1.327 | 1.344 | 1.362 | 1.379 |
| 16 | 1.396 | 1.414 | 1.431 | 1.449 | 1.467 | 1.485 | 1.503 | 1.521 | 1.539 | 1.558 |
| 17 | 1.576 | 1.595 | 1.614 | 1.632 | 1.651 | 1.670 | 1.689 | 1.709 | 1.728 | 1.748 |
| 18 | 1.767 | 1.787 | 1.807 | 1.827 | 1.847 | 1.867 | 1.887 | 1.907 | 1.928 | 1.948 |
| 19 | 1.969 | 1.990 | 2.011 | 2.032 | 2.053 | 2.074 | 2.095 | 2.117 | 2.138 | 2.160 |
| 20 | 2.182 | 2.204 | 2.226 | 2.248 | 2.270 | 2.292 | 2.315 | 2.337 | 2.360 | 2.382 |
| 21 | 2.405 | 2.428 | 2.451 | 2.474 | 2.498 | 2.521 | 2.545 | 2.568 | 2.592 | 2.616 |
| 22 | 2.640 | 2.664 | 2.688 | 2.712 | 2.737 | 2.761 | 2.786 | 2.810 | 2.835 | 2.860 |
| 23 | 2.885 | 2.910 | 2.936 | 2.961 | 2.986 | 3.012 | 3.038 | 3.064 | 3.089 | 3.115 |
| 24 | 3.142 | 3.168 | 3.194 | 3.221 | 3.247 | 3.274 | 3.301 | 3.328 | 3.355 | 3.382 |
| 25 | 3.409 | 3.436 | 3.464 | 3.491 | 3.519 | 3.547 | 3.574 | 3.602 | 3.631 | 3.659 |
| 26 | 3.687 | 3.715 | 3.744 | 3.773 | 3.801 | 3.830 | 3.859 | 3.888 | 3.917 | 3.947 |
| 27 | 3.976 | 4.006 | 4.035 | 4.065 | 4.095 | 4.125 | 4.155 | 4.185 | 4.215 | 4.246 |
| 28 | 4.276 | 4.307 | 4.337 | 4.368 | 4.399 | 4.430 | 4.461 | 4.493 | 4.524 | 4.555 |
| 29 | 4.587 | 4.619 | 4.650 | 4.682 | 4.714 | 4.746 | 4.779 | 4.811 | 4.844 | 4.876 |
| 30 | 4.909 | 4.942 | 4.974 | 5.007 | 5.041 | 5.074 | 5.107 | 5.140 | 5.174 | 5.208 |
| 31 | 5.241 | 5.275 | 5.309 | 5.343 | 5.378 | 5.412 | 5.446 | 5.481 | 5.515 | 5.550 |
| 32 | 5.585 | 5.620 | 5.655 | 5.690 | 5.726 | 5.761 | 5.796 | 5.832 | 5.868 | 5.904 |
| 33 | 5.940 | 5.976 | 6.012 | 6.048 | 6.084 | 6.121 | 6.158 | 6.194 | 6.231 | 6.268 |
| 34 | 6.305 | 6.342 | 6.379 | 6.417 | 6.454 | 6.492 | 6.529 | 6.567 | 6.605 | 6.643 |
| 35 | 6.681 | 6.720 | 6.758 | 6.796 | 6.835 | 6.874 | 6.912 | 6.951 | 6.990 | 7.029 |
| 36 | 7.069 | 7.108 | 7.147 | 7.187 | 7.227 | 7.266 | 7.306 | 7.346 | 7.386 | 7.426 |
| 37 | 7.467 | 7.507 | 7.548 | 7.588 | 7.629 | 7.670 | 7.711 | 7.752 | 7.793 | 7.834 |
| 38 | 7.876 | 7.917 | 7.959 | 8.001 | 8.042 | 8.084 | 8.126 | 8.169 | 8.211 | 8.253 |
| 39 | 8.296 | 8.338 | 8.381 | 8.424 | 8.467 | 8.510 | 8.553 | 8.596 | 8.640 | 8.683 |
| 40 | 8.727 | 8.770 | 8.814 | 8.858 | 8.902 | 8.946 | 8.990 | 9.035 | 9.079 | 9.124 |
| 41 | 9.168 | 9.213 | 9.258 | 9.303 | 9.348 | 9.393 | 9.439 | 9.484 | 9.530 | 9.575 |
| 42 | 9.621 | 9.667 | 9.713 | 9.759 | 9.805 | 9.852 | 9.898 | 9.945 | 9.991 | 10.038 |
| 43 | 10.085 | 10.132 | 10.179 | 10.226 | 10.273 | 10.321 | 10.368 | 10.416 | 10.463 | 10.511 |
| 44 | 10.559 | 10.607 | 10.655 | 10.704 | 10.752 | 10.801 | 10.849 | 10.898 | 10.947 | 10.996 |
| 45 | 11.045 | 11.094 | 11.143 | 11.192 | 11.242 | 11.291 | 11.341 | 11.391 | 11.441 | 11.491 |
| 46 | 11.541 | 11.591 | 11.642 | 11.692 | 11.743 | 11.793 | 11.844 | 11.895 | 11.946 | 11.997 |
| 47 | 12.048 | 12.100 | 12.151 | 12.203 | 12.254 | 12.306 | 12.358 | 12.410 | 12.462 | 12.514 |
| 48 | 12.566 | 12.619 | 12.671 | 12.724 | 12.777 | 12.830 | 12.882 | 12.936 | 12.989 | 13.042 |
| 49 | 13.095 | 13.149 | 13.203 | 13.256 | 13.310 | 13.364 | 13.418 | 13.472 | 13.527 | 13.581 |
| 50 | 13.635 | 13.690 | 13.745 | 13.800 | 13.854 | 13.909 | 13.965 | 14.020 | 14.075 | 14.131 |

II

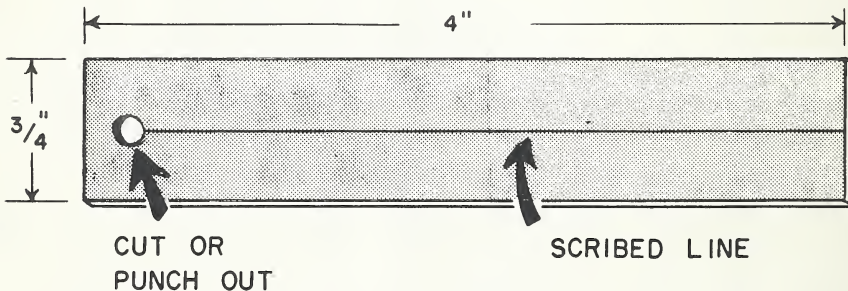
Circular Slide Rule A is used for determining cubic volume in 8-foot butt sections.

III

Circular Slide Rule B is used for determining cubic volume in upper logs, 16-foot length.

For convenience in use, both Slide Rules A and B are inserted unbound in this paper. Each consists of two parts, a base and a movable wheel. To assemble, cut out the movable wheel and fasten it to the base with a metal grommet, binder post, or pin. The centers are marked. The slide rules can be stiffened and made more durable by covering both parts with clear acetate.

Use of a finder made from a piece of stiff clear acetate will increase accuracy and reduce the time required to locate the volume opposite the desired butt-diameter reading. The diagram below can be used as a pattern for making such a finder.



The size of the hole punched or cut out of the finder will depend on the size of the grommet or pin used in assembling the parts of the circular slide rule.

Directions for use of the slide rules are printed on the movable wheel of each.

IV

Table 2.--Cubic-foot volume of single-stem tree tops

(Truncated at fixed 4-inch top d.i.b. only)

b = butt d.i.b.

$$\begin{aligned} \text{Formula for cone frustrum: Vol.} &= \frac{[4^2 + b(b+4)]}{3} \left(\frac{\pi}{4:144} \right) L \\ &= [16 + b(b+4)] (0.001818) L \end{aligned}$$

| Butt diameter (inches, inside bark) | Length (feet) | | | | | | | | | | | | |
|--|---------------|------|------|------|------|------|------|------|------|------|-------|-------|-------|
| | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 5.0 | 0.44 | 0.55 | 0.67 | 0.78 | 0.89 | 1.00 | 1.11 | 1.22 | 1.33 | 1.44 | 1.55 | 1.66 | 1.77 |
| 5.5 | .50 | .62 | .74 | .87 | .99 | 1.12 | 1.24 | 1.36 | 1.49 | 1.61 | 1.74 | 1.86 | 1.99 |
| 6.0 | .55 | .69 | .83 | .97 | 1.11 | 1.24 | 1.38 | 1.52 | 1.66 | 1.80 | 1.93 | 2.07 | 2.21 |
| 6.5 | .61 | .77 | .92 | 1.07 | 1.23 | 1.38 | 1.53 | 1.68 | 1.84 | 1.99 | 2.14 | 2.30 | 2.45 |
| 7.0 | .68 | .85 | 1.01 | 1.18 | 1.35 | 1.52 | 1.69 | 1.86 | 2.03 | 2.20 | 2.37 | 2.54 | 2.71 |
| 7.5 | .74 | .93 | 1.12 | 1.30 | 1.49 | 1.67 | 1.86 | 2.04 | 2.23 | 2.42 | 2.60 | 2.79 | 2.97 |
| 8.0 | .81 | 1.02 | 1.22 | 1.43 | 1.63 | 1.83 | 2.04 | 2.24 | 2.44 | 2.65 | 2.85 | 3.05 | 3.26 |
| 8.5 | .89 | 1.11 | 1.33 | 1.56 | 1.78 | 2.00 | 2.22 | 2.44 | 2.67 | 2.89 | 3.11 | 3.33 | 3.56 |
| 9.0 | .97 | 1.21 | 1.45 | 1.69 | 1.93 | 2.18 | 2.42 | 2.66 | 2.90 | 3.14 | 3.39 | 3.63 | 3.87 |
| 9.5 | 1.05 | 1.31 | 1.57 | 1.84 | 2.10 | 2.36 | 2.62 | 2.88 | 3.15 | 3.41 | 3.67 | 3.93 | 4.20 |
| 10.0 | 1.13 | 1.42 | 1.70 | 1.99 | 2.27 | 2.55 | 2.84 | 3.12 | 3.40 | 3.69 | 3.97 | 4.25 | 4.54 |
| 10.5 | 1.22 | 1.53 | 1.84 | 2.14 | 2.45 | 2.75 | 3.06 | 3.36 | 3.67 | 3.98 | 4.28 | 4.59 | 4.89 |
| 11.0 | 1.32 | 1.65 | 1.97 | 2.30 | 2.63 | 2.96 | 3.29 | 3.62 | 3.95 | 4.28 | 4.61 | 4.94 | 5.26 |
| 11.5 | 1.41 | 1.77 | 2.12 | 2.47 | 2.83 | 3.18 | 3.53 | 3.88 | 4.24 | 4.59 | 4.94 | 5.30 | 5.65 |
| 12.0 | 1.51 | 1.89 | 2.27 | 2.65 | 3.03 | 3.40 | 3.78 | 4.16 | 4.54 | 4.92 | 5.29 | 5.67 | 6.05 |
| 12.5 | 1.62 | 2.02 | 2.42 | 2.83 | 3.23 | 3.64 | 4.04 | 4.44 | 4.85 | 5.25 | 5.66 | 6.06 | 6.46 |
| 13.0 | 1.72 | 2.15 | 2.59 | 3.02 | 3.45 | 3.88 | 4.31 | 4.74 | 5.17 | 5.60 | 6.03 | 6.46 | 6.89 |
| 13.5 | 1.83 | 2.29 | 2.75 | 3.21 | 3.67 | 4.13 | 4.59 | 5.04 | 5.50 | 5.96 | 6.42 | 6.88 | 7.34 |
| 14.0 | 1.95 | 2.44 | 2.92 | 3.41 | 3.90 | 4.39 | 4.87 | 5.36 | 5.85 | 6.33 | 6.82 | 7.31 | 7.80 |
| 14.5 | 2.07 | 2.58 | 3.10 | 3.62 | 4.13 | 4.65 | 5.17 | 5.68 | 6.20 | 6.72 | 7.23 | 7.75 | 8.27 |
| 15.0 | 2.19 | 2.74 | 3.28 | 3.83 | 4.38 | 4.92 | 5.47 | 6.02 | 6.57 | 7.11 | 7.66 | 8.21 | 8.76 |
| 15.5 | 2.31 | 2.89 | 3.47 | 4.05 | 4.63 | 5.21 | 5.79 | 6.36 | 6.94 | 7.52 | 8.10 | 8.68 | 9.26 |
| 16.0 | 2.44 | 3.05 | 3.67 | 4.28 | 4.89 | 5.50 | 6.11 | 6.72 | 7.33 | 7.94 | 8.55 | 9.16 | 9.77 |
| 16.5 | 2.58 | 3.22 | 3.86 | 4.51 | 5.15 | 5.80 | 6.44 | 7.08 | 7.73 | 8.37 | 9.02 | 9.66 | 10.30 |
| 17.0 | 2.71 | 3.39 | 4.07 | 4.75 | 5.42 | 6.10 | 6.78 | 7.46 | 8.14 | 8.82 | 9.49 | 10.17 | 10.85 |
| 17.5 | 2.85 | 3.57 | 4.28 | 4.99 | 5.70 | 6.42 | 7.13 | 7.84 | 8.56 | 9.27 | 9.98 | 10.70 | 11.41 |
| 18.0 | 3.00 | 3.75 | 4.49 | 5.24 | 5.99 | 6.74 | 7.49 | 8.24 | 8.99 | 9.74 | 10.49 | 11.24 | 11.98 |

